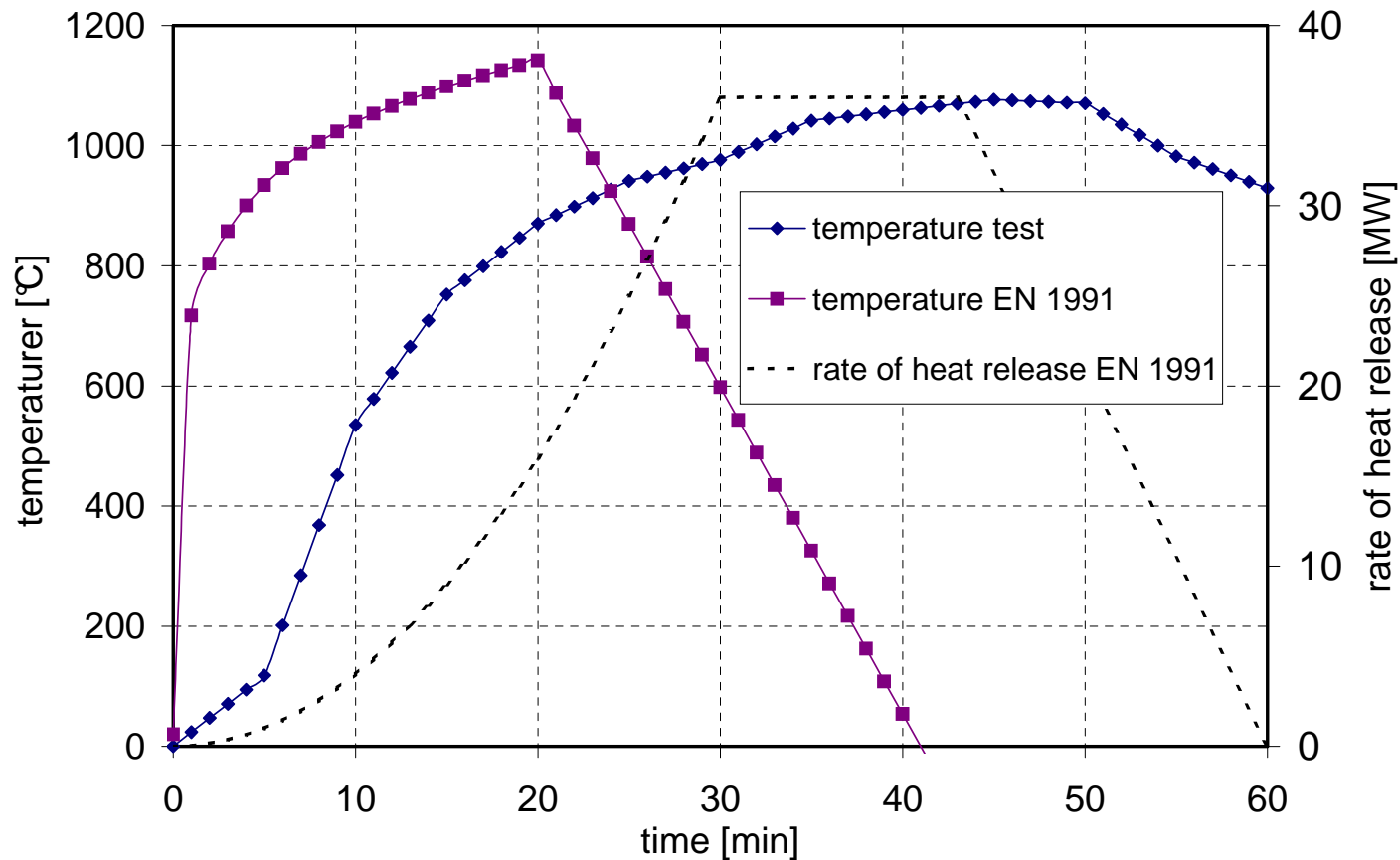


▷ CASE STUDIES OF A NEW SIMPLIFIED NATURAL FIRE MODEL AND SAFETY CONCEPT FOR STRUCTURAL FIRE SAFETY DESIGN

Dr.-Ing. Jochen Zehfuss
Head of Hamburg branch
hhpberlin Fire Safety Engineers

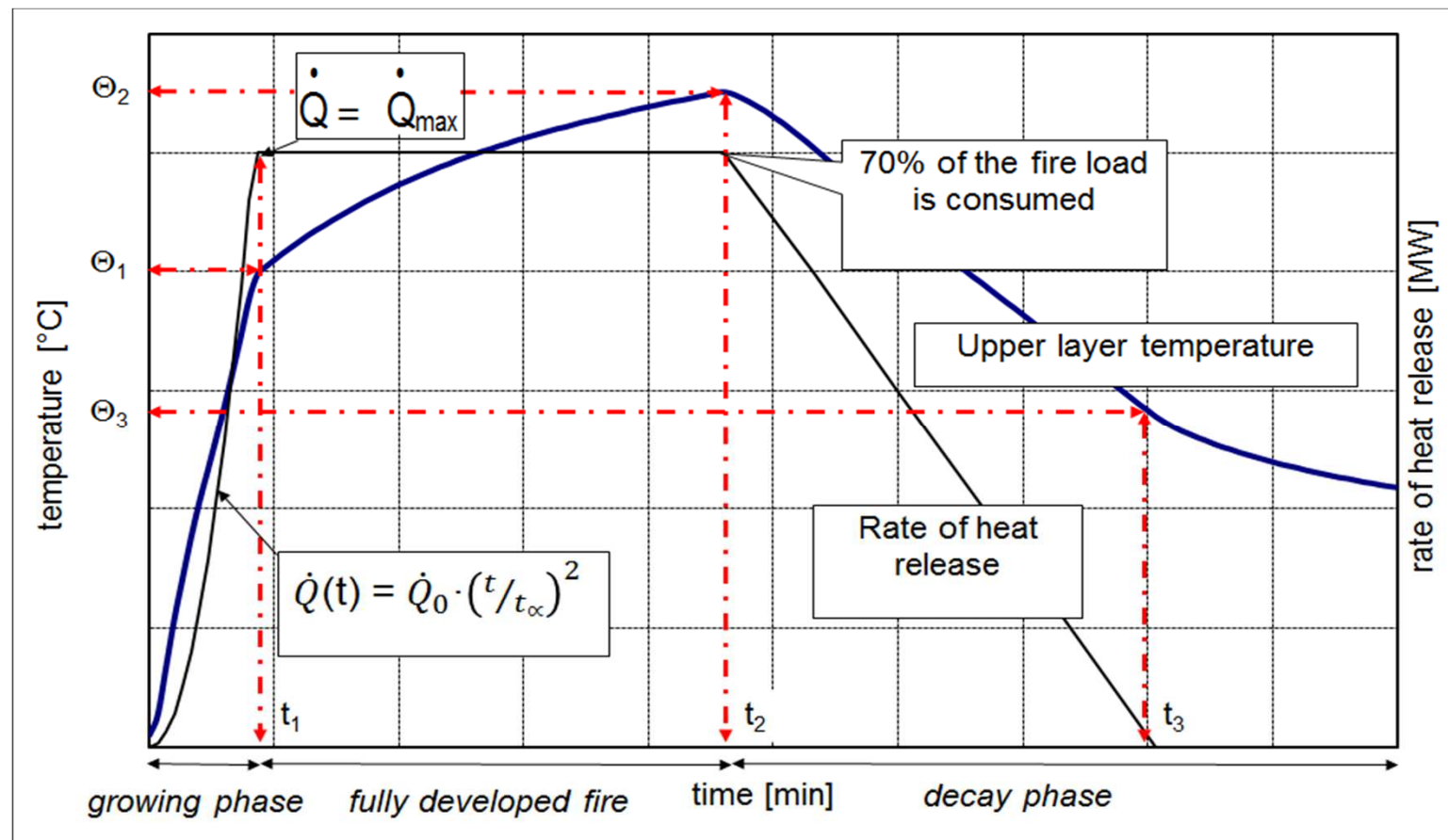
Parametric curves EN 1991-1-2



no temporal correlation between RHR and parametric curves



➤ Approach of parametric fire curves

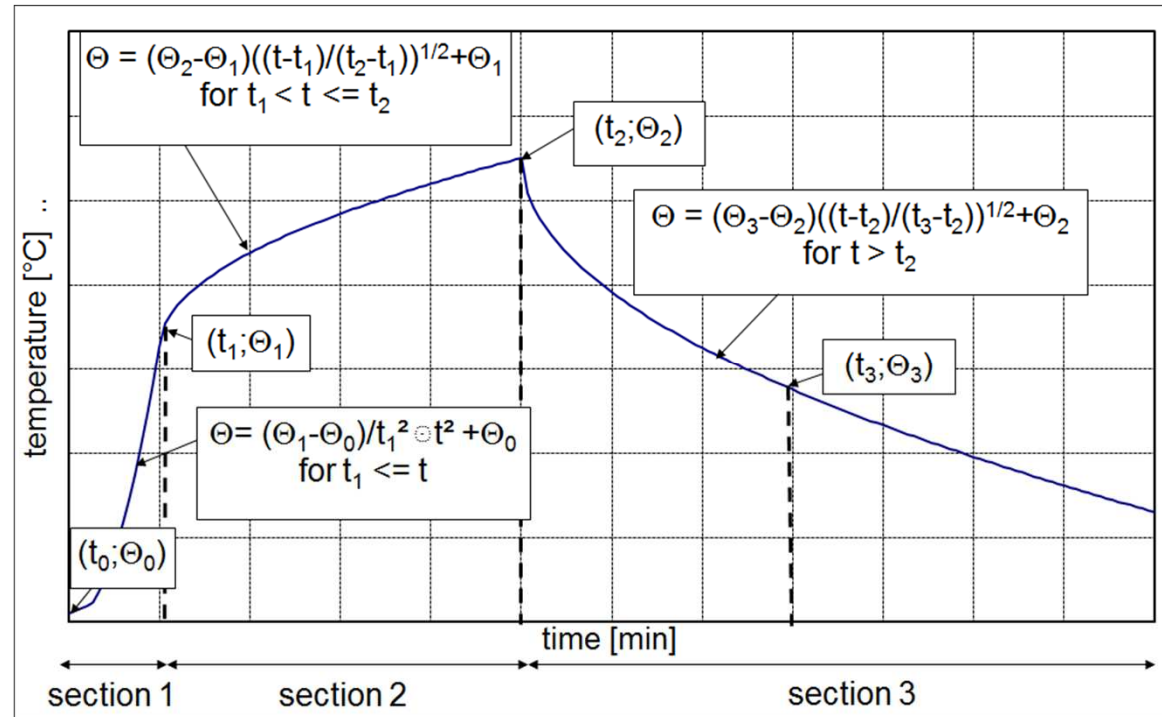


➤ Parametric fire curves vent.-contr.

$$\Theta_1 = -8.75 \cdot 1/O - 0.1 b + 1175 \text{ [}^\circ\text{C]}$$

$$\Theta_2 = (0.004 b - 17) \cdot 1/O - 0.4 b + 2175 \text{ [}^\circ\text{C]}$$

$$\Theta_3 = -5.0 \cdot 1/O - 0.16 b + 1060 \text{ [}^\circ\text{C]}$$



with

opening factor

area of ventilation openings

averaged height of ventilation openings

total area of enclosing components

averaged thermal property of enclosure

$$O = A_w \sqrt{h_w} / A_t \text{ [m}^{1/2}\text{]},$$

$$A_w \text{ [m}^2\text{]},$$

$$h_w \text{ [m]},$$

$$A_t \text{ [m}^2\text{]},$$

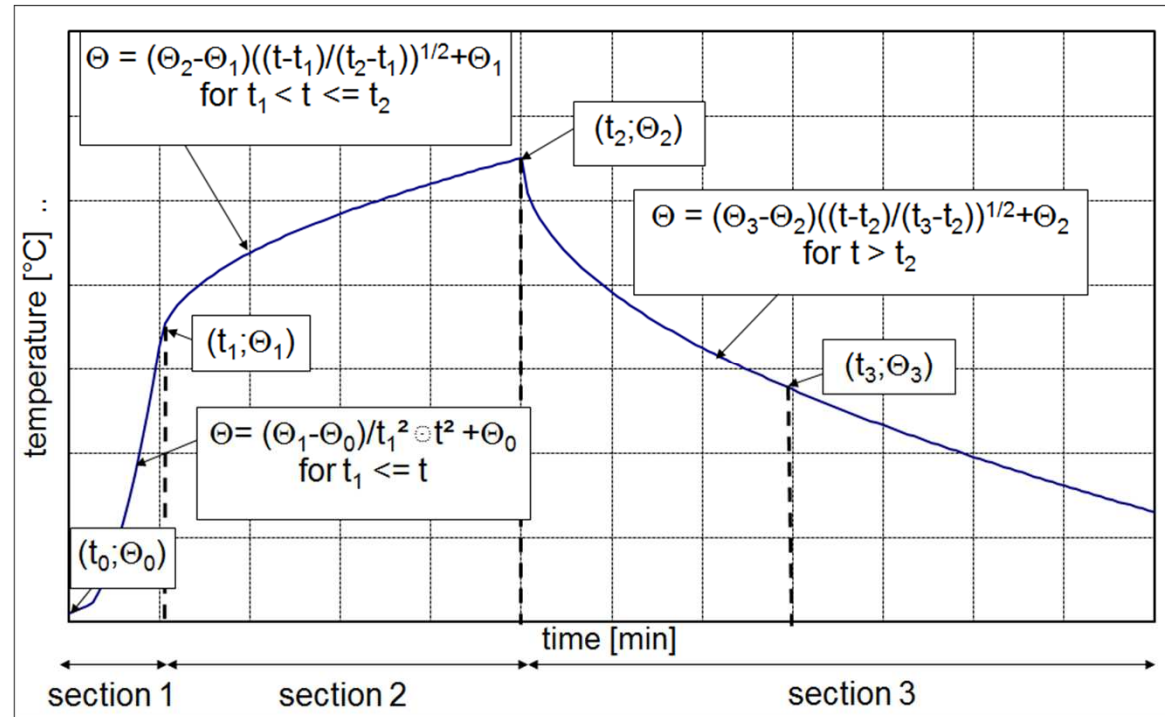
$$b \text{ [J/m}^2\text{s}^{0.5}\text{K]}.$$

➤ Parametric fire curves fuel-contr.

$$\Theta_1 = 24000 k + 20 \text{ [}^\circ\text{C]}$$

$$\Theta_2 = 33000 k + 20 \text{ [}^\circ\text{C]}$$

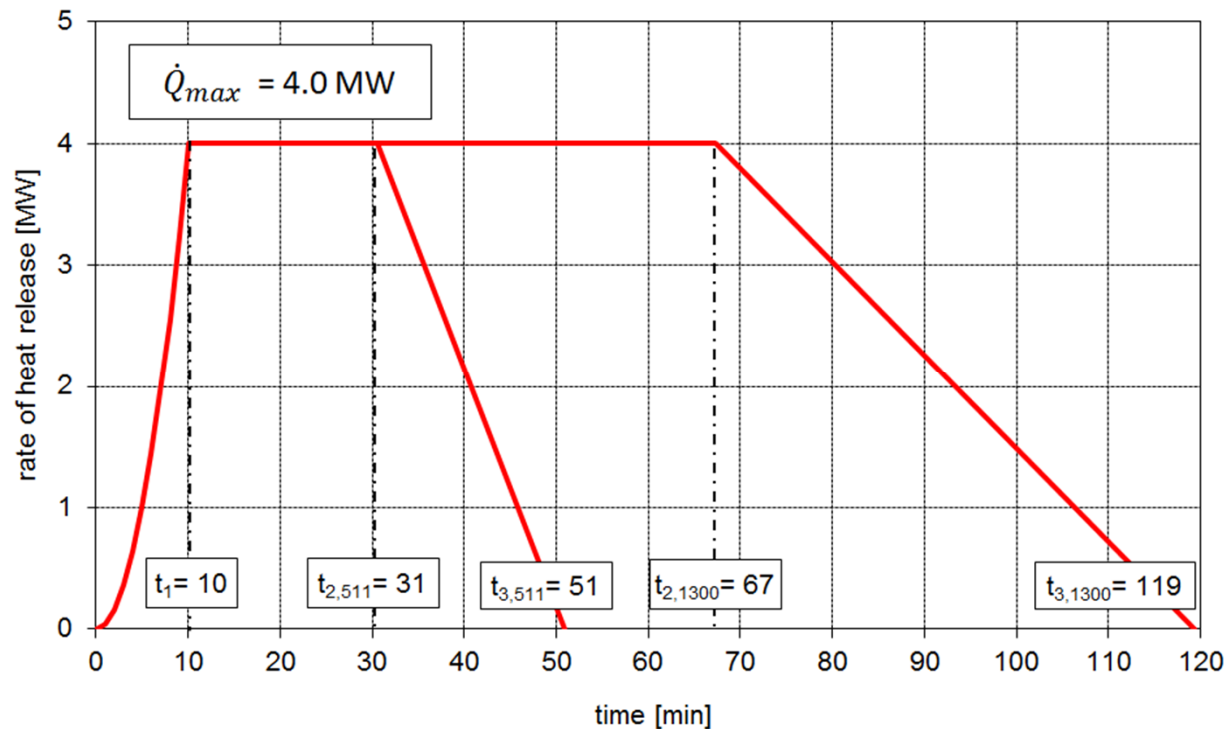
$$\Theta_3 = 16000 k + 20 \text{ [}^\circ\text{C]}$$



$$k = \left(\frac{\dot{Q}_{\max, f}^2}{A_w \sqrt{h_w} \cdot A_T \cdot b} \right)^{1/3}$$

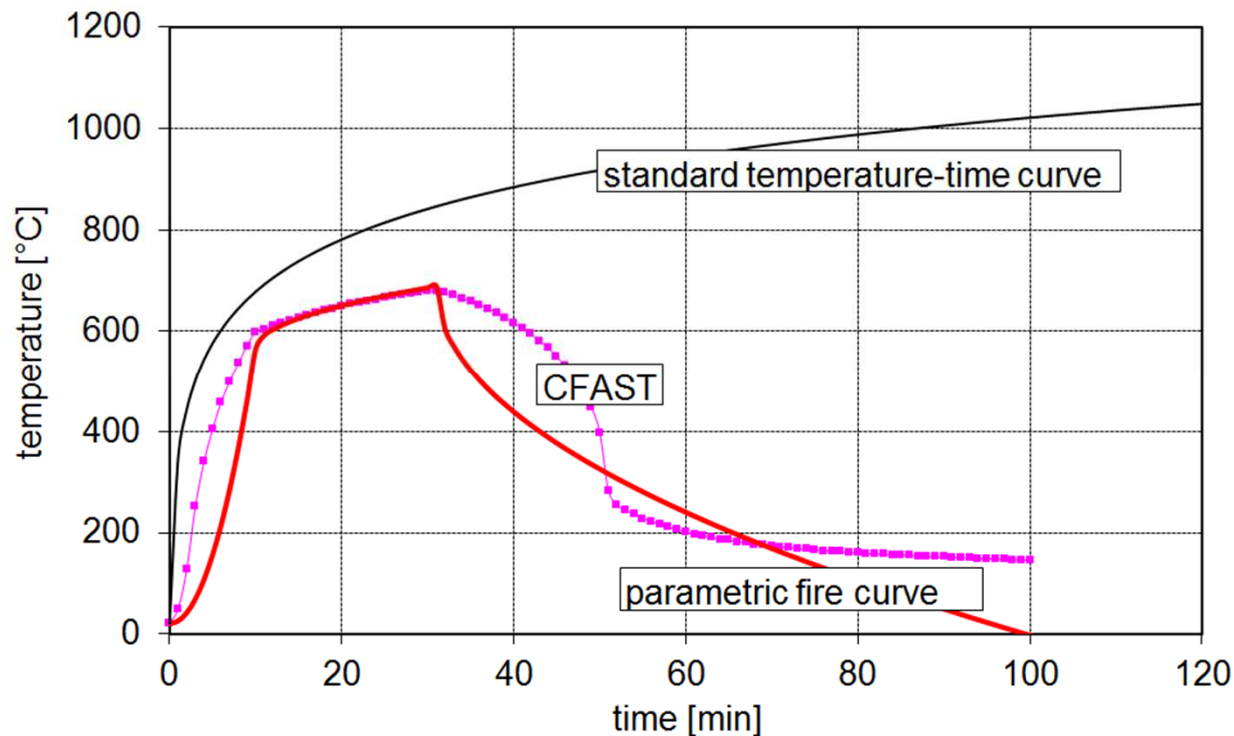
➤ Example of application

| | | | |
|--|---|----------------------------|-----------------------------|
| Floor area of fire compartment | $A_f = 16 \text{ m}^2$, | Height of fire compartment | $H = 3.00 \text{ m}$ |
| Area of openings | $A_w = 8.0 \text{ m}^2$, | Averaged opening height | $h_w = 2.50 \text{ m}^2$ |
| Ventilation factor | $A_w \sqrt{h_w} = 12.65 \text{ m}^{3/2}$ | Opening factor | $O = 0.158 \text{ m}^{1/2}$ |
| Total area of the enclosing components | $A_t = 80.0 \text{ m}^2$ | | |
| Fire load density $q_x = 511 \text{ MJ/m}^2$ | $Q_{511} = 8176 \text{ MJ}$ | | |
| averaged thermal property of enclosure | $b = 1500 \text{ J}/(\text{m}^2\text{s}^{0,5}\text{K})$ | | |



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