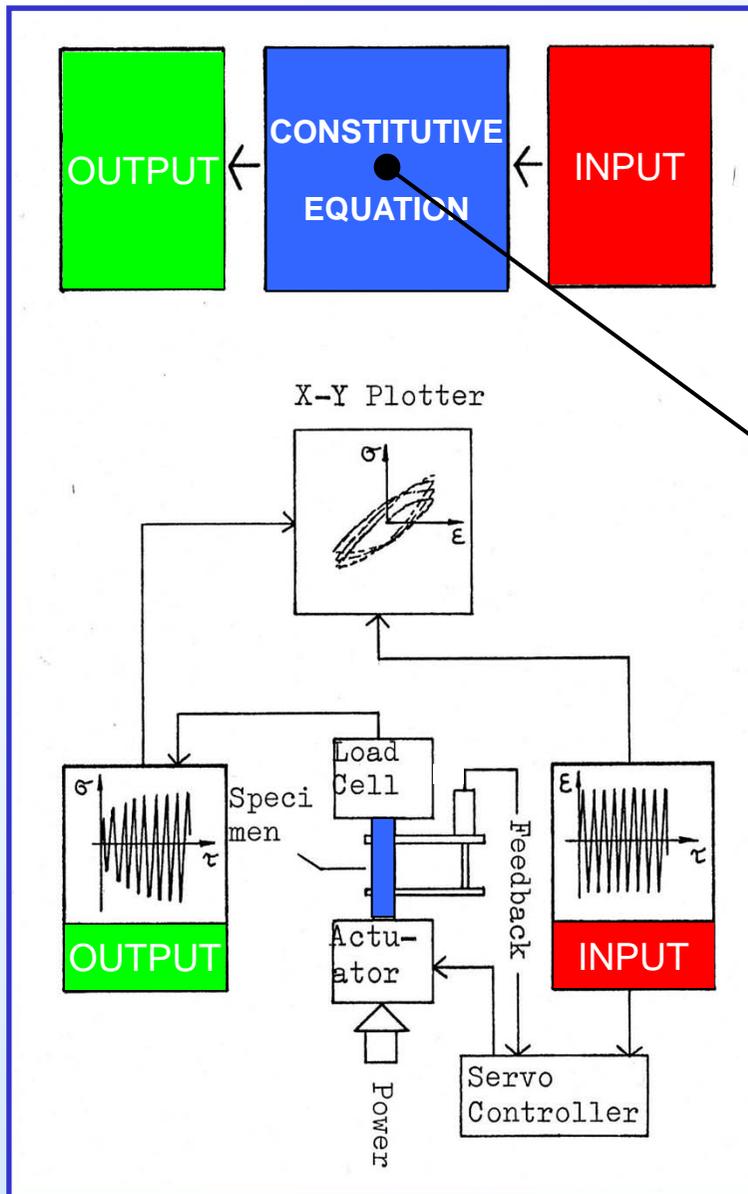


Constitutive Equations for Structural Steel Subjected to Fire: Some Remarks

M. KORZEN

BAM Federal Institut for Materials Research and Testing,
Division *Fire Engineering*,
Berlin, Germany

Operator view on material and constitutive equation



σ : Stress, ε : Strain, θ : Temperature

- F Operator

$$\sigma(t) = F \left(\varepsilon(\tau), \theta(\tau) \right)_{0 \leq \tau \leq t}$$

- $\varepsilon(\tau), \theta(\tau)$ Input function (Loading)
- $\sigma(t)$ Output function (Response)

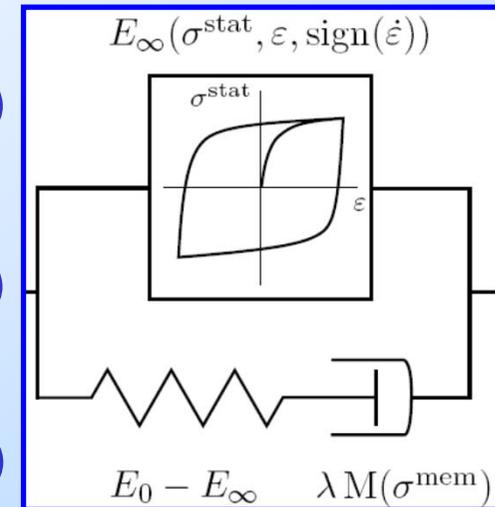
Example of a *constitutive model*



$$\dot{\sigma} = -\frac{1}{\lambda(\theta, \sigma - \sigma^{stat})} [\sigma - \sigma^{stat}] + E_0(\theta) \dot{\varepsilon}^{mech} \quad (1)$$

$$\dot{\sigma}^{stat} = g(\theta, \text{sign}(\dot{\varepsilon}^{mech}), \varepsilon^{mech}, \sigma^{stat}) \dot{\varepsilon}^{mech} \quad (2)$$

$$\varepsilon^{mech} := \varepsilon - \alpha(\theta) [\theta - \theta_0] \quad (3)$$



- Derived from 3-parameter solid of viscoelasticity with modifications:
 - Strain replaced by mechanical strain
 - Linear elastic static stress replaced by rate-independent hysteresis
 - Dependence of all material parameters on temperature
 - Dependence of relaxation time on the difference between stress and static stress
- (1) – (3) **unified** constitutive model, no separate creep and plastic strain
- (1) – (3) define an **ODE** system of type: $\underline{\dot{y}} = \underline{h}(\underline{y}(t), t), \underline{y}(0) = \underline{y}_0$

- *Transient creep* is material response to special loading functions, i.e.

$$L_{\sigma}(\tau) = \sigma(\tau) = \sigma^* = \text{const.} \quad (4)$$

and

$$L_{\theta}(\tau) = \theta(\tau) = \dot{\theta}^* \tau, \dot{\theta}^* = \text{const.} \quad (5)$$

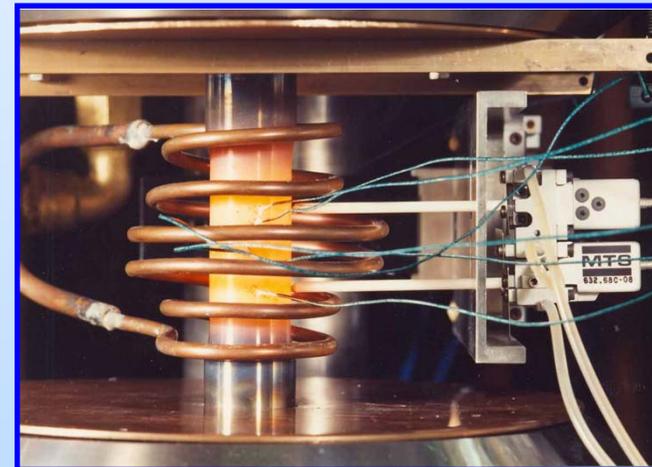
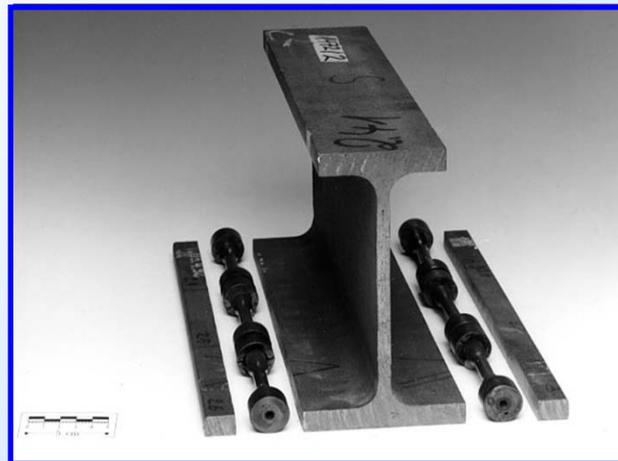
$$\dot{\varepsilon}^{mech} = \frac{\sigma^* - \sigma^{stat}}{\lambda(\theta, \sigma^* - \sigma^{stat}) E_0(\theta)} \quad (6)$$

$$\dot{\sigma}^{stat} = g(\theta, \text{sign}(\dot{\varepsilon}^{mech}), \varepsilon^{mech}, \sigma^{stat}) \dot{\varepsilon}^{mech} \quad (7)$$

- Constitutive model as an operator to run numerical simulations via software package *RADAU* for different values of σ^* and $\dot{\theta}^*$

Results on poster: Figures 4, 5 and 6 !

- Special transient creep test:
 - Compression Loading: -100 MPa
 - LCF specimen produced from flange of an IPB 180 section, S235 steel

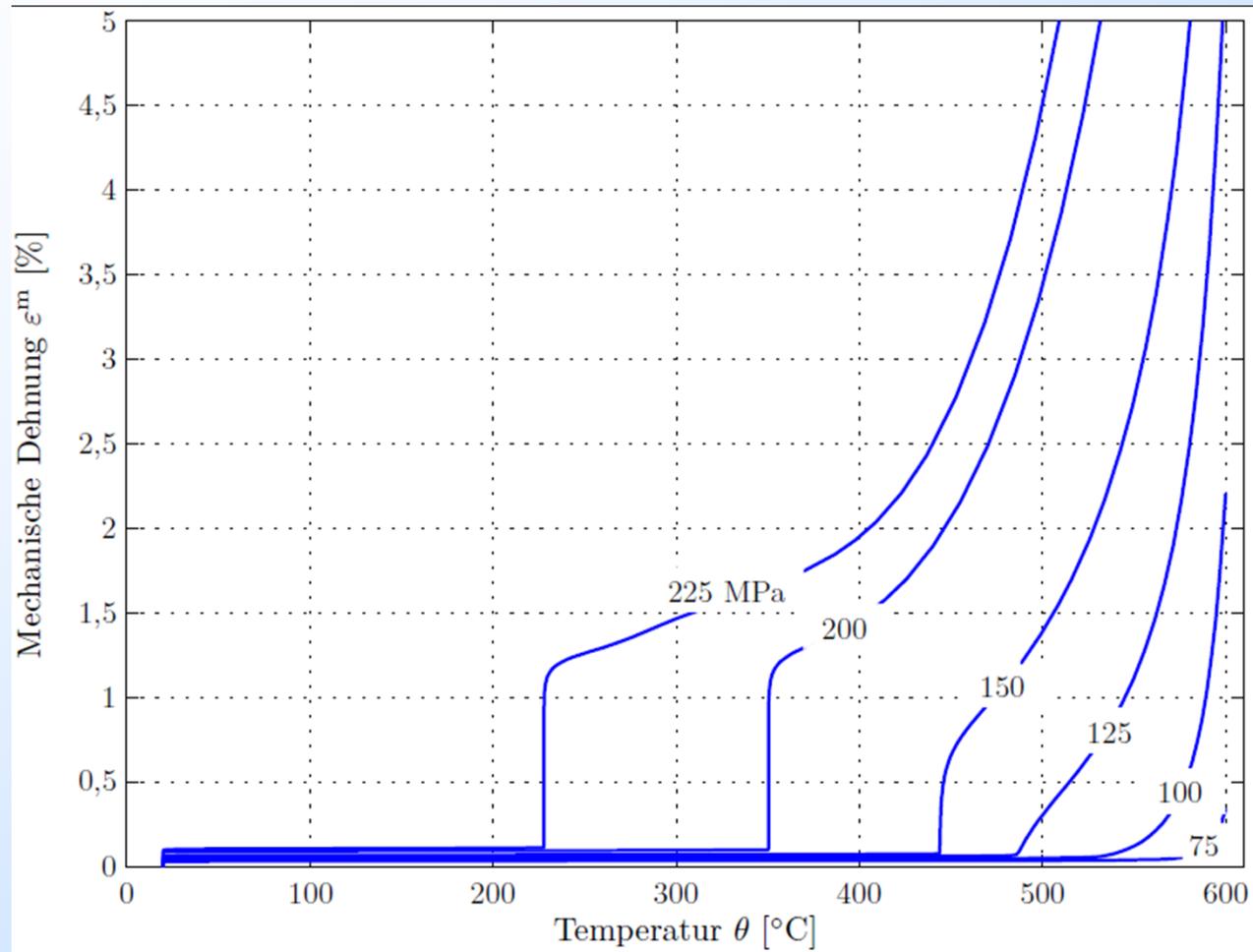


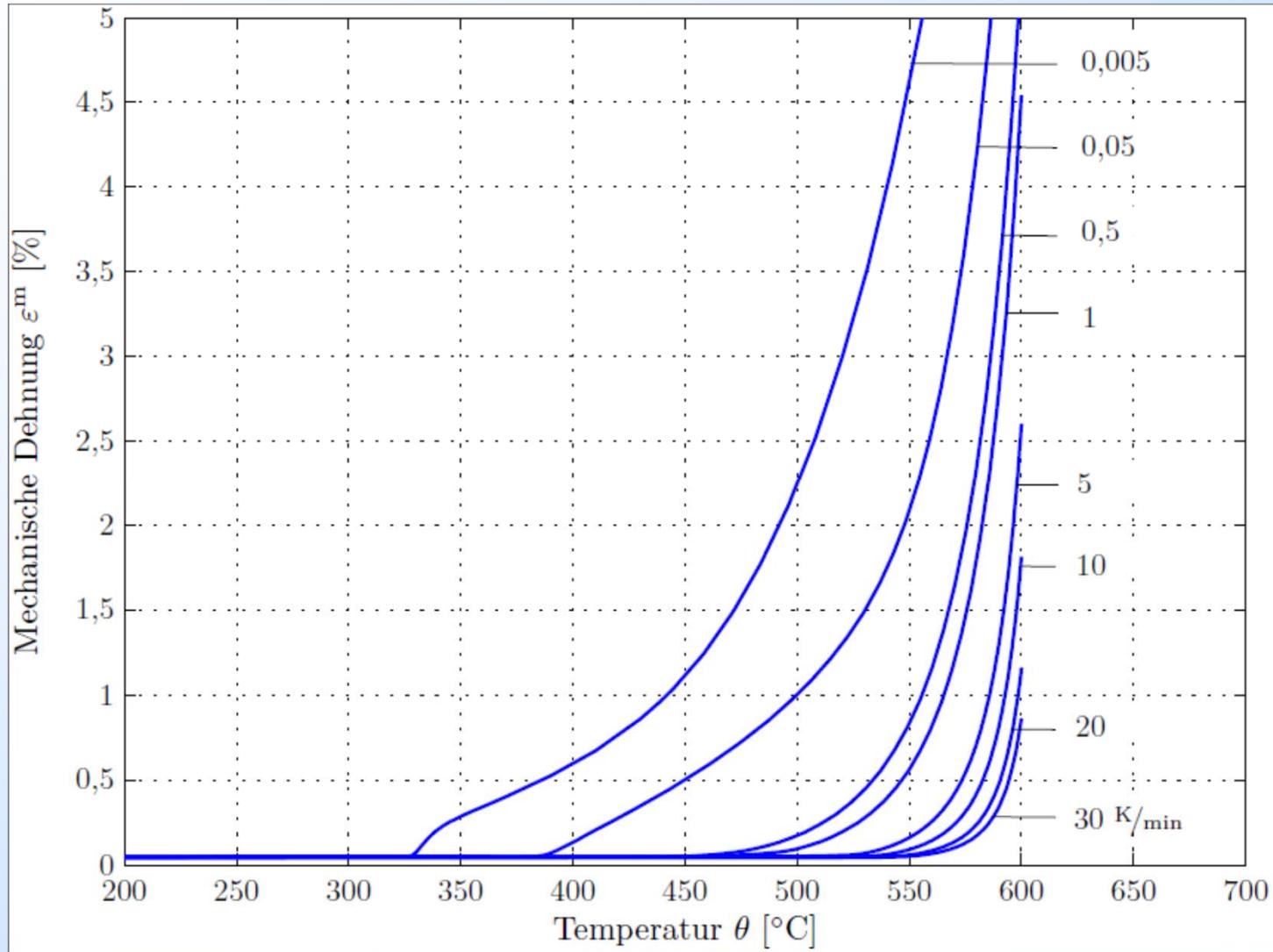
- Non-monotonic heating through high-frequency inductive coils at 7 K/min

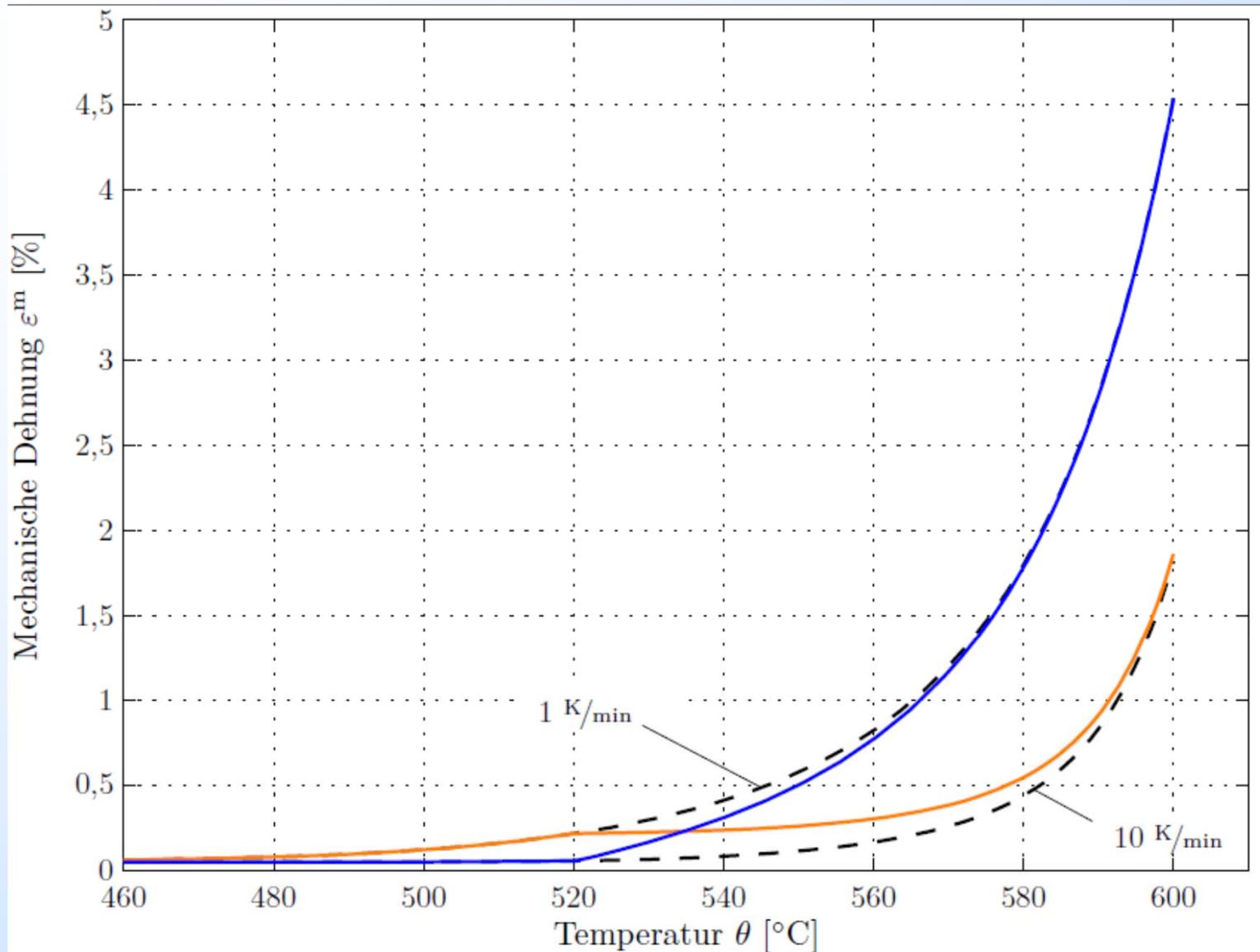
Results on poster: Figure 7 !

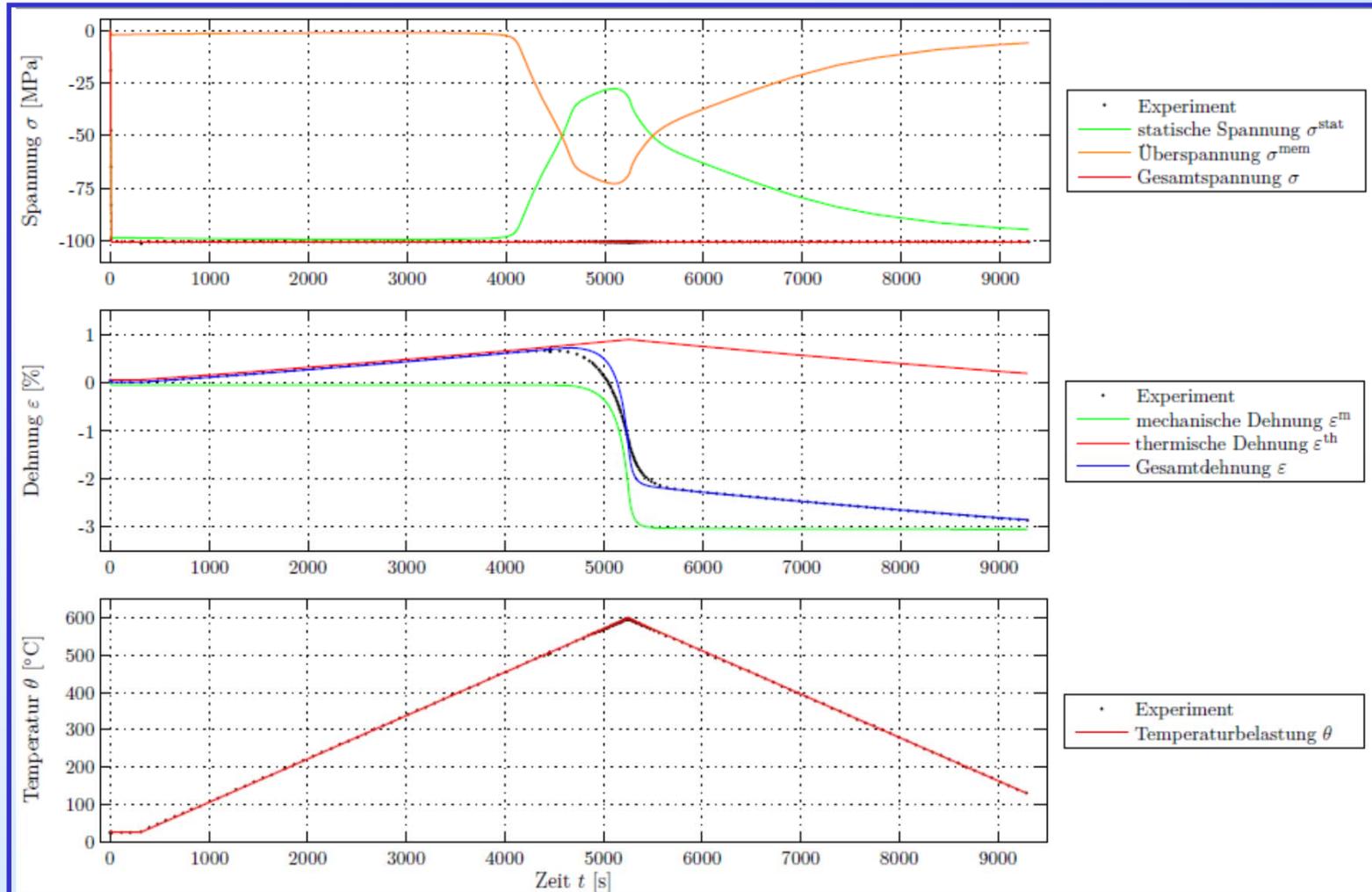
Thank you for your attention

Acknowledgements: The author is very grateful to Dipl.-Ing. Le Trung Nguyen who has done all simulations including its visualisations.









$$\dot{\sigma} = -\frac{1}{\lambda(\theta, \sigma - \sigma^{stat})} [\sigma - \sigma^{stat}] + E_0(\theta) \dot{\varepsilon}^{mech}, \sigma(0) = 0$$

$$\dot{\sigma}^{stat} = g(\theta, \text{sign}(\dot{\varepsilon}^{mech}), \varepsilon^m, \sigma^{stat}) \dot{\varepsilon}^{mech}, \sigma^{stat}(0) = 0$$

$$g(\cdot) := E_e(\theta) \frac{\beta(\theta) E_e(\theta) - \text{sign}(\dot{\varepsilon}^{mech}) [\sigma^{stat} - E_p(\theta) \varepsilon^{mech}]}{\beta(\theta) E_e(\theta) - \kappa(\theta) \text{sign}(\dot{\varepsilon}^{mech}) [\sigma^{stat} - E_p(\theta) \varepsilon^{mech}]}$$

$$\varepsilon^{mech} := \varepsilon - \alpha(\theta) [\theta - \theta_0]$$

$$\dot{y} = \underline{h}(y(t), t), y(0) = y_0$$

$$\dot{\varepsilon}^{mech} = \frac{\sigma^* - \sigma^{stat}}{\lambda(\theta, \sigma - \sigma^{stat}) E_0(\theta)}, \varepsilon^{mech}(0) = 0$$

$$\dot{\sigma}^{stat} = g(\theta, \text{sign}(\dot{\varepsilon}^{mech}), \varepsilon^{mech}, \sigma^{stat}) \dot{\varepsilon}^{mech}, \sigma^{stat}(0) = 0$$