Overview of the development of fire engineering in research and practice

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Various methods for determining the fire resistance.

- 1. Experimental Tests
- 2. Tabulated data
- 3. Simple calculation models
- 4. Advanced calculation models

Method 1: Experimental testing

Testing specimens for material behaviour



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Method 1: Experimental testing

- >Testing material behaviour
- ►Standard fire tests.
 - Circumstancial disadvantages: cost, delays, limited # of facilities.
 - Real disadvantages: only elements, size of the element,

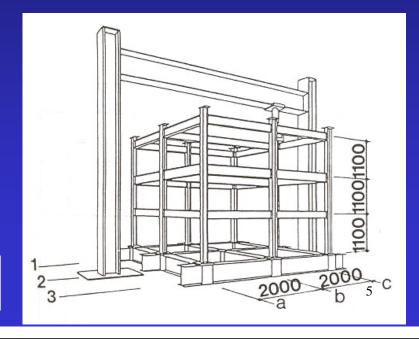
boundary conditions, variability.



Method 1: Experimental testing

- **➤**Testing material behaviour
- >Standard fire tests
- **▶**Small scale fire tests

Steel: OK
Hydral materials: ???



Picture from Nakamura et al., 1^{rst} IAFSS, Gaithersburg, 1985

Method 1: Experimental testing

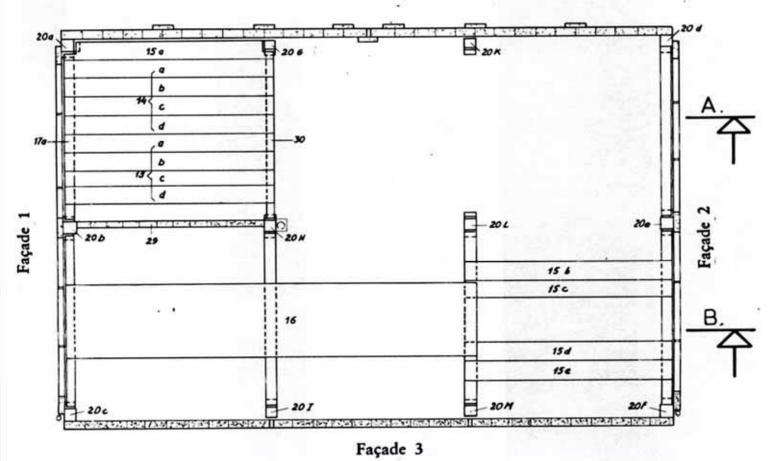
- >Testing material behaviour
- >Standard fire tests
- >Small scale fire tests
- >Large scale fire tests

Rare - Local fires - Observations more than research



Concrete building- Gent

Façade 4







- ⇒Experimental testing is used mainly in research.
- ⇒Experimental testing will remain forever.
 - •Verification of basic hypotheses used in calculation models
 - •Integrity criteria in separating elements



Method 2: Tabulated data

Definition: presentation, in simple form, of results obtained by other methods.

Standard fire resistance	Minimum dimensions (mm)					
	Slab		Axis-distance <i>a</i>			
	thickness h_s	One way Two way		way		
			$l_y/l_x \le 1.5$	$1.5 < l_y/l_x \le 2$		
1	2	3	4	5		
REI 30	60	10*	10*	10*		
REI 60	80	20	10*	15*		
REI 90	100	30	15*	20		
REI 120	120	40	20	25		
REI 180	150	55	30	40		
REI 240	175	65	40	50		

 l_y and l_x are the spans of a two-way slab where l_y is the longer span. For prestressed slabs the increase of axis distance should be noted.

The axis distance a in Column 4 and 5 for two way slabs relate to slabs supported on all four edges. Otherwise, they should be treated as one-way spanning slabs.

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Method 2: Tabulated data

Reinforcement ratio $\omega = 0.50$; Eccentricity $\mathbf{e} \le 200 \text{ mm}$								
Standard fire	λ	Column width b_{min} / axis distance a						
resistance		n = 0.15	n = 0.30	n = 0.50	n = 0.70			
R30	30	150/25*	150/25*	250/35:300/25*	500/40:550/25*			
	40	150/25*	150/30:200/25*	300/35:450/25*	550/30			
	50	150/25*	200/30:250/25*	400/40:500/25*	550/50:600/40			
	60	150/25*	200/35:300/25*	450/50:550/25*	(1)			
	70	150/25*	250/40:400/25*	500/40:600/30*	(1)			
	80	150/25*	300/40:500/25*	550/50:600/40*	(1)			
R 60	30	150/30:200/25*	200:40:450/25*	450/50:550/30	550/50:600/40			
	40	150/35:250/25*	250:40:500/25*	500/40:550/35	600/60			
	50	200/35:300/25*	300:45:550/25*	500/55:550:40	(1)			
	60	200/40:500/25*	400:40:600/30	550/50:600/45	(1)			
	70	200/40:550/25*	500:40:550/35	600/60	(1)			
	80	250/40:600/25*	500:40:600/35	(1)	(1)			
R 90	30	250/40:450/25*	300/50:500/25	500/55:600/40	600/80			
	40	200/50:500/25*	350/50:550/35	550/60:600/50	(1)			
	50	250/45:550/25*	500/45:550/40	600/60	(1)			
	60	250/50:550/30	500/50:550/45	600/80	(1)			
	70	300/50:550/35	550/50:600/45	(1)	(1)			
	80	350/50:600/35	550/60:600/50	(1)	(1)			

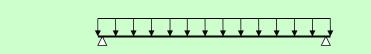
^{*} Normally the cover at room conditions will control (1) Requires a width greater than 600 mm.

^{*} Normally the cover required at room temperature will control

Method 3: Simple calculation models

Definition: Method based on global equilibrium conditions.

$$\begin{array}{rcl}
M_{\text{max}} & \leq & R_d \\
\frac{q L^2}{8} & \leq & W_{pl} f_y
\end{array}$$



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Method 3: Simple calculation models

- Extrapolations of similar methods used at room temperature
- Can be used « by hand »
- One method for each material/member type.
- Not well suited for complex structures.

=> Used for real projects.

At
$$20^{\circ}C$$
: $\frac{q_d L^2}{8} \leq W_{pl} f_y$

At high temperature:
$$\frac{q_{d,fi} L^2}{8} \le W_{pl} f_y(T)$$

Method 4: Advanced calculation models

Definition: Based on principles of structural mechanics or of heat transfer (local equations).

$$\frac{\partial \sigma_{xx}}{\partial x} + \frac{\partial \sigma_{xy}}{\partial y} + \frac{\partial \sigma_{xz}}{\partial z} + F_x = 0$$

$$\frac{\partial \sigma_{yx}}{\partial x} + \frac{\partial \sigma_{yy}}{\partial y} + \frac{\partial \sigma_{yz}}{\partial z} + F_y = 0$$

$$\frac{\partial \sigma_{zx}}{\partial x} + \frac{\partial \sigma_{zy}}{\partial y} + \frac{\partial \sigma_{zz}}{\partial z} + F_z = 0$$

$$\lambda \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + Q - c\rho \frac{\partial T}{\partial t} = 0$$

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Method 4: Advanced calculation models

- Finite differences, finite elements, boundary elements.
- Require a computer (numerical calculation models).

- 1. 'My Ph.D.' software
 - One author (university)



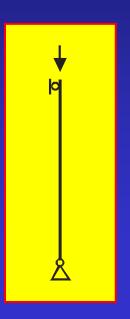
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Method 4 : Advanced calculation models

Three different families of software:

- 1. 'My Ph.D.' software
 - One author (university)
 - Limited field of application





1. 'My Ph.D.' software

- **One author (university)**
- Limited field of application
- **Limited availability**



Method 4: Advanced calculation models

Three different families of software:

1. 'My Ph.D.' software

- **One author (university)**
- Limited field of application
- Limited availability



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- 1. 'My Ph.D.' software
- 2. Dedicated software (VULCAN, SAFIR,...)
 - From a group (University)



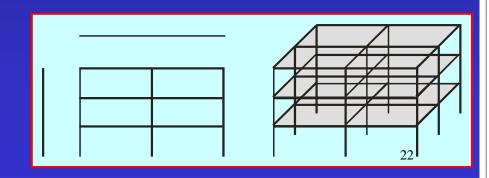
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Method 4: Advanced calculation models

Three different families of software:

- 1. 'My Ph.D.' software
- 2. Dedicated software (VULCAN, SAFIR,...)
 - From a group (University)
 - Wider field of application



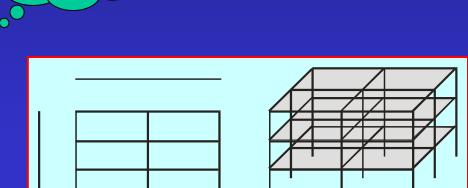


- 1. 'My Ph.D.' software
- 2. Dedicated software (VULCAN, SAFIR,...)

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- From a group (University)
- Wider field of application
- Become available now





Method 4: Advanced calculation models

Three different families of software:

- 1. 'My Ph.D.' software
- 2. Dedicated software (VULCAN, SAFIR,...)
- 3. Commercial software (ANSYS, ABAQUS,...)
 - · Widely distributed, used and validated
 - Price !!!
 - Nice graphics

+++ or ---

What can we model and what should we test?

Which material can we model?

A priori, all of them...

if we have the properties.

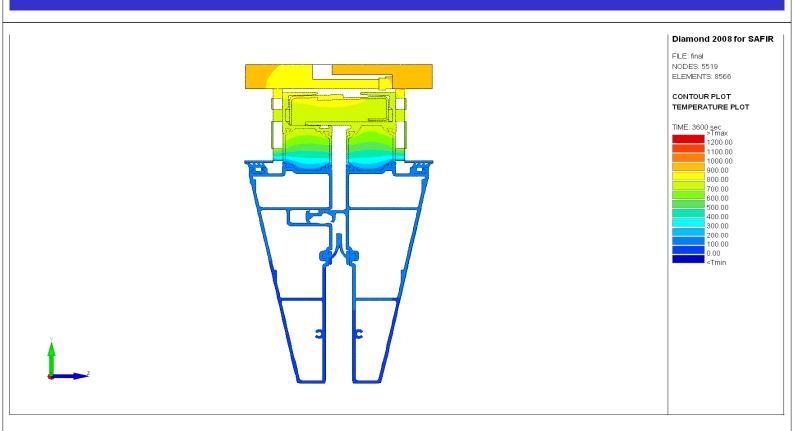
Which properties?

Properties of the material?

No. Properties of the model.

=> Know the limits of your model.

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Window frame (courtesy: Permasteelisa)

What can we model and what should we test?

Which structure can we model?

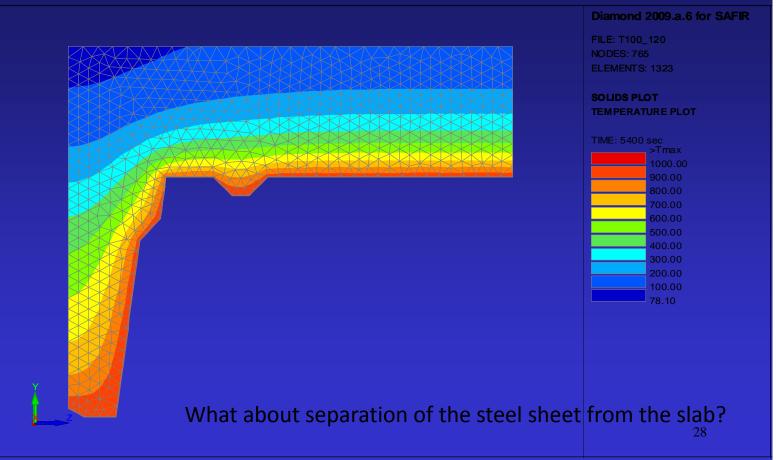
A priori, none of them...

except if we made a test before on a similar structure.

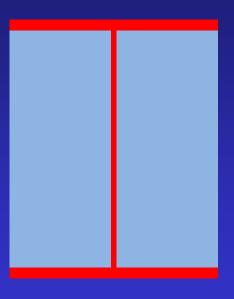
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examples

1) Composite floor on corrugated steel sheets

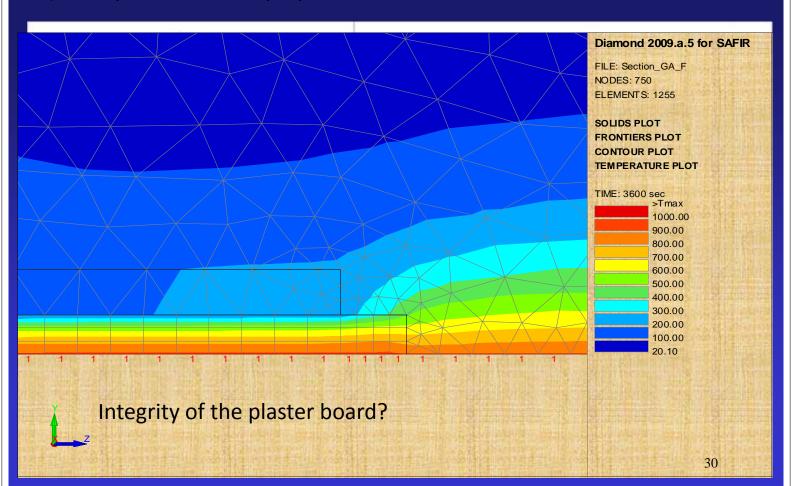


2) Composite steel concrete columns

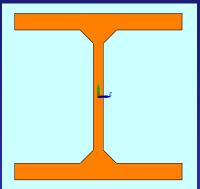


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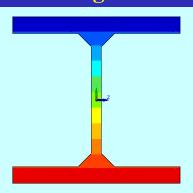
3) Steel plate covered by a plaster board



Yesterday Uniform temperature



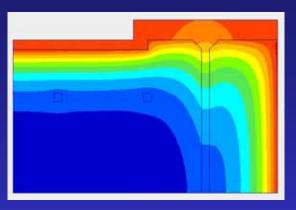
Linear gradient

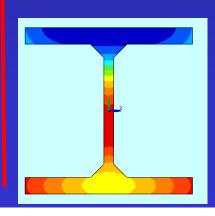


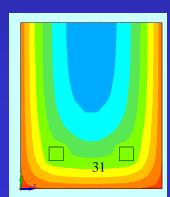
Method 4 : Advanced calculation models

Today

Non uniform temperature





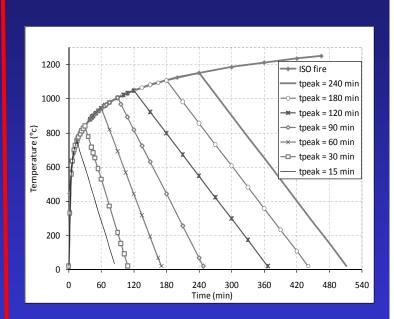


Yesterday ISO fire

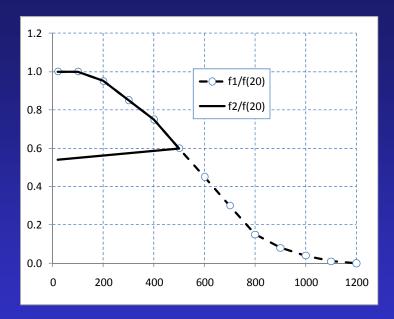
Method 4 : Advanced calculation models

Today

Natural fires (with cooling phase)

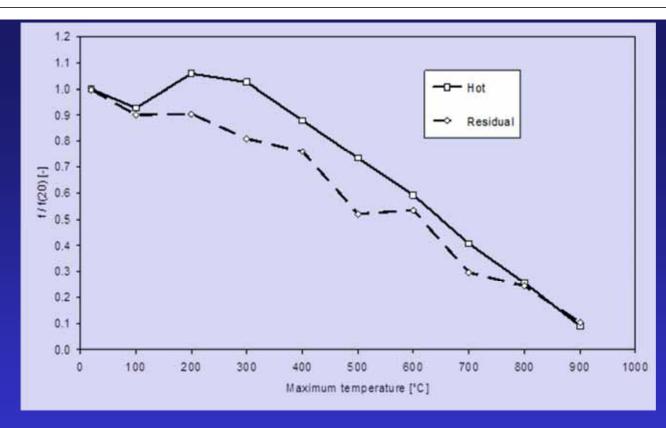


Requires specific material models.



Compressive strength of concrete





Difference between hot and residual compressive strength From Li & Franssen, Journal of Structural Fire Engineering, 2(1), 2011, 29-44.



Collapse of an undergroud car park after the fire has been put 35down

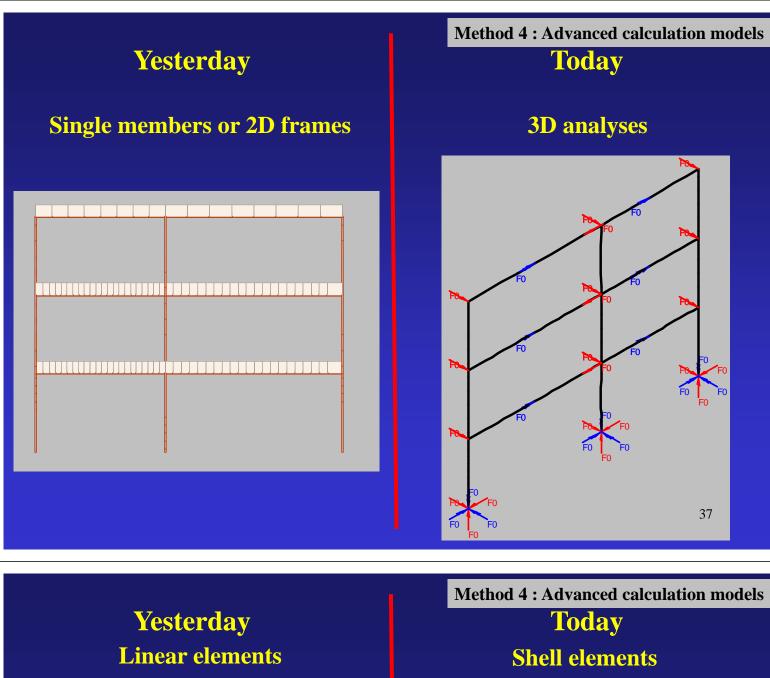
Yesterday

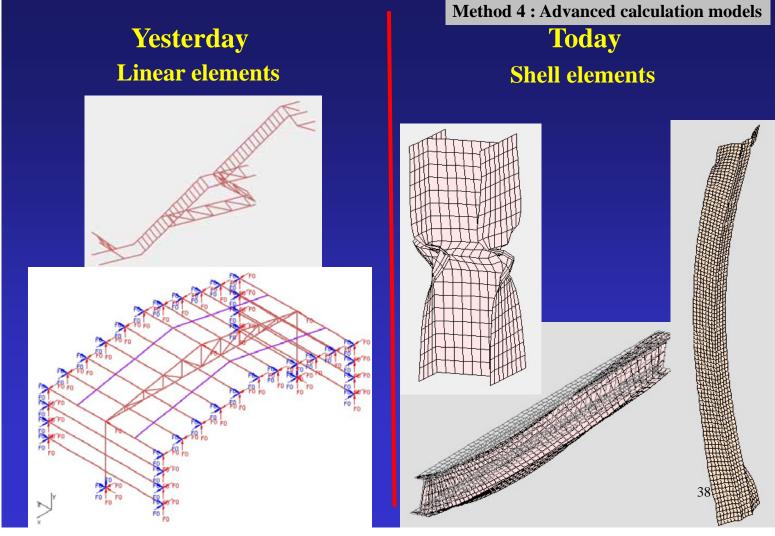
Implicit transient creep

Method 4 : Advanced calculation models

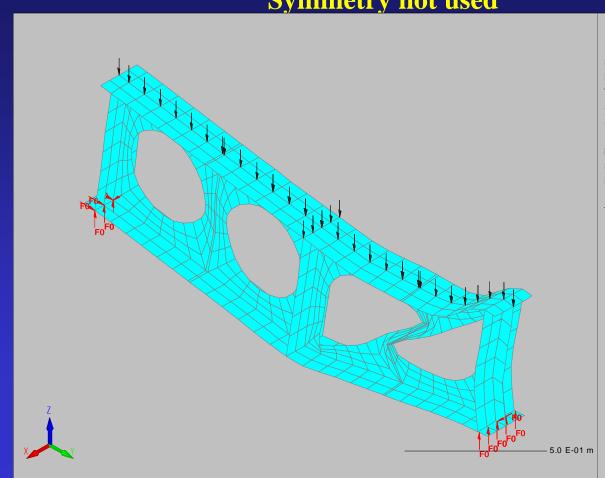
Today

Explicit transient creep





Short Cellular Steel beam Symmetry not used



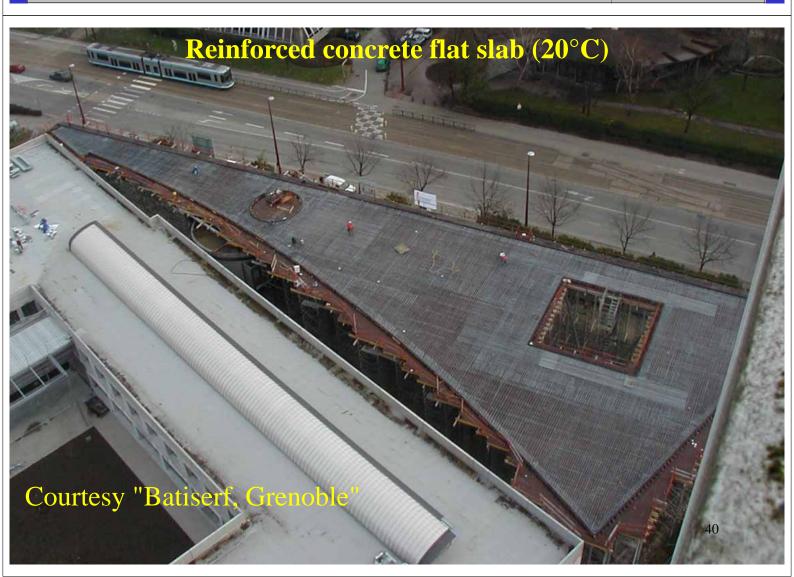
Diamond 2004 for SAFIR

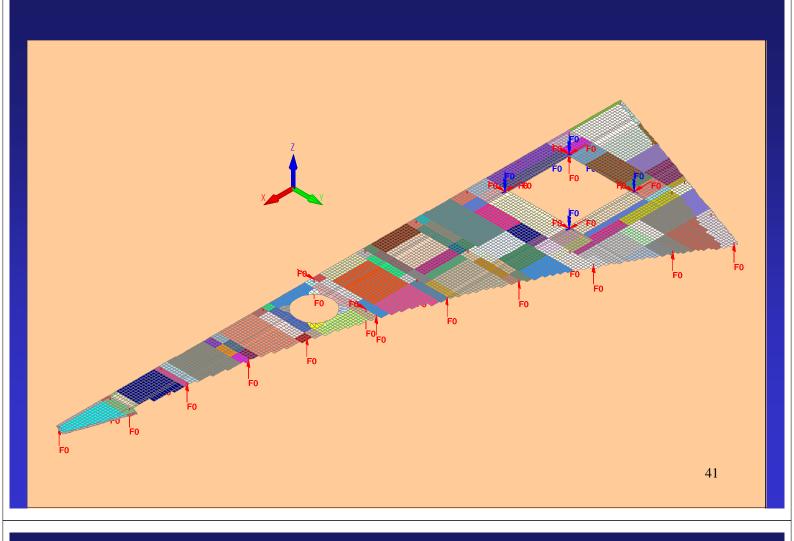
FILE: acb_dyn_hot NODES: 905 BEAMS: 0 TRUSSES: 0 SHELLS: 608 SOILS: 0

IMPOSED DOF PLOT POINT LOADS PLOT DISPLACEMENT PLOT (x 1)

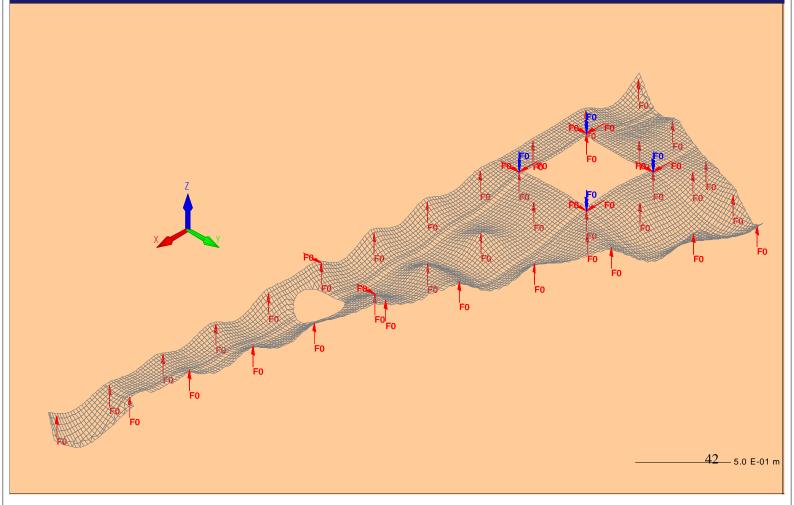
TIME: 651.1728 sec

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Displacement in the ultimate limit state

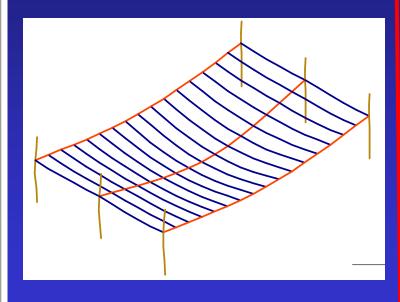


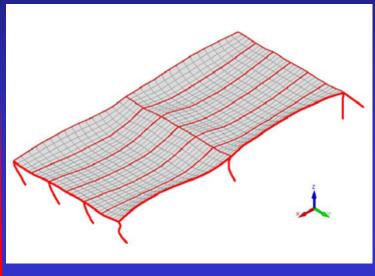
Yesterday

One type of F.E.

Method 4 : Advanced calculation models Today

Several types of F.E.





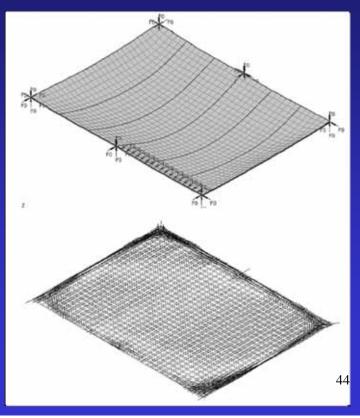
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Yesterday

One way bending in floors

Method 4 : Advanced calculation models Today

Tensile membrane action



Yesterday

Static analyses

$$\{\Delta F\} = [K]\{\Delta u\}$$

Method 4 : Advanced calculation models Today

Dynamic analyses

$${F} = [K]{u} + [C]{\overset{\bullet}{u}} + [M]{\overset{\bullet}{u}}$$

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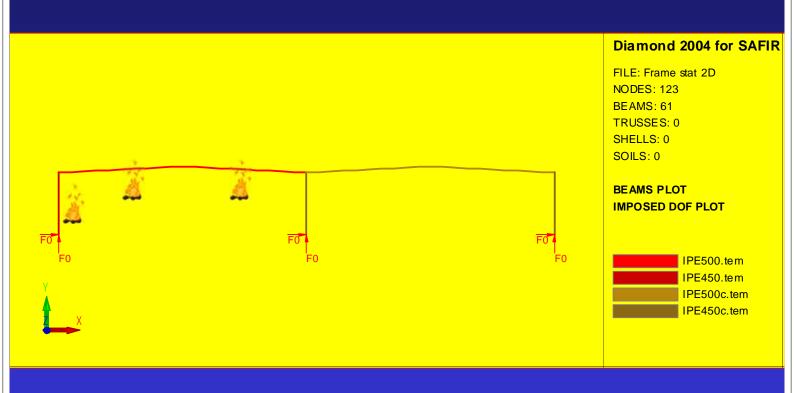
Lee's Frame Analysed with Shell F.E. in bending $dT/dt = 1^{\circ}C/s$

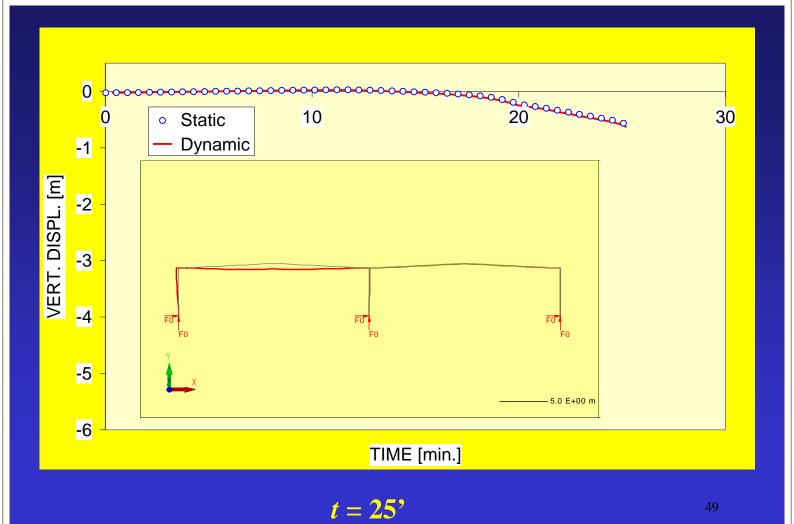


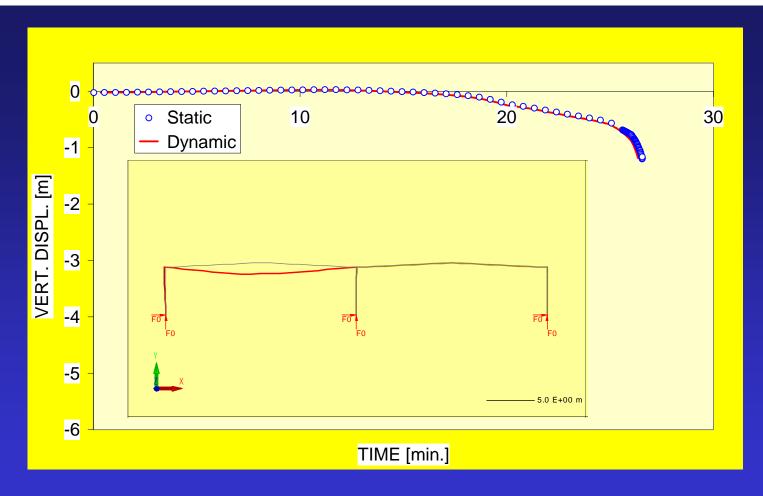
Other considerations

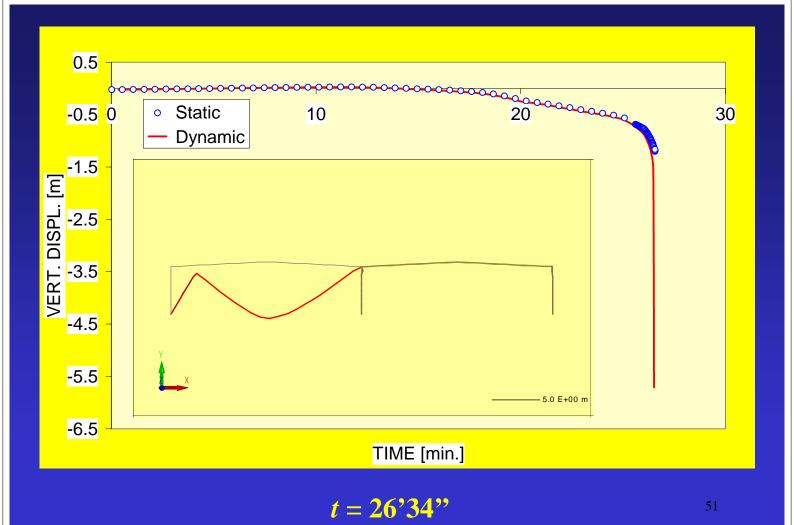
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Failure mode may be more critical than time of collapse











The same, now in 3D, with heated purlins

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Diamond XL for S LOCAL FIRE ON 3D FILE: Animation NODES: 1223 BEAMS: 585 TRUSSES: 0 SHELLS: 0 DISPLACEMENT PL TIME: 20,97152 sec

3D frame (no amplification in the deformation)

When performing a S.i.F. analysis:

- ✓ make it simple,
- ✓ or not,

but not both.

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Natural fire with cooling phase.

Criteria?

- ❖ Time of collapse (natural fire) > required time for evacuation
- ❖ Infinite resistance (until complete burn out)?
- ightharpoonup Time of collapse (natural fire) = R(ISO) ?

Stupidity?

Or maybe not!

Representation of the fire?

Nominal fire curve?

OK for structural research in the heating phase

Post-flashover parametric fire curve?

OK for structural research with a cooling phase

Zone models?

Ok if the geometry is appropriate

Difficulty for the columns in multi zone models

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Representation of the fire?

Local models (Hasemi)?

OK if the geometry is appropriate Hasemi not applicable for columns

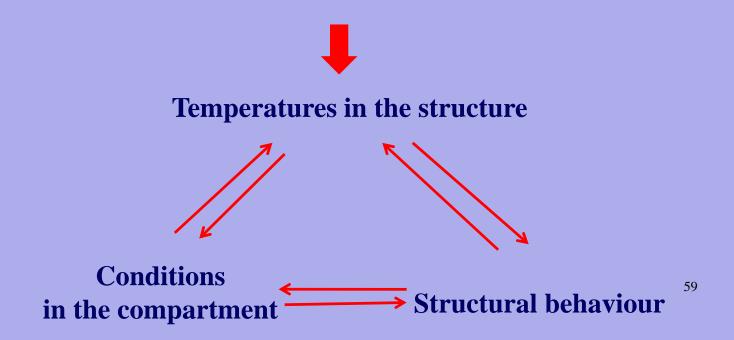
CFD

Not for post-flashover fires

OK when local fire, large compartment with complex geometry, big budget.

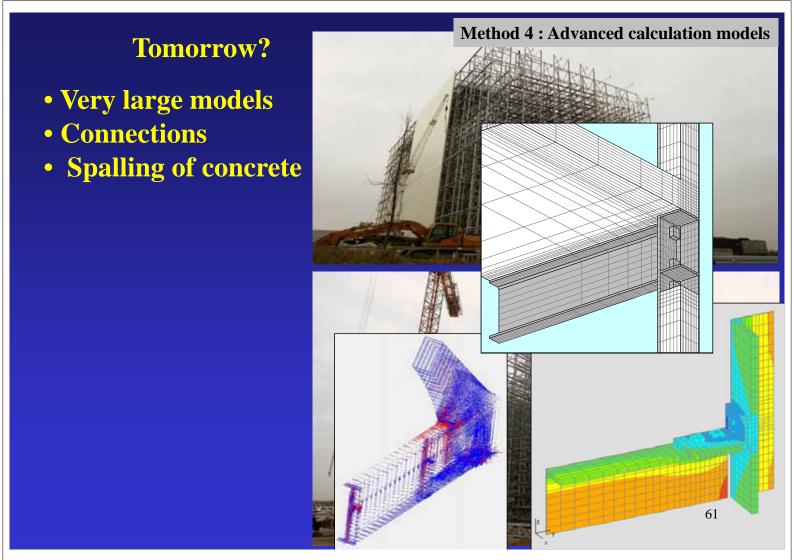
Which interactions to consider?

IN REALITY EVERYTHING IS COUPLED



Structural fire engineering used in practice to:

- 1) Prove stability without any protection on steel
- 2) Reduce fire protection on steel
- 3) Prove fire resistance of existing concrete structure
- 4) Prove failure mode





Tomorrow?

• C.F.D. - F.E. interconnection

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Method 4: Advanced calculation models

Tomorrow

- Moisture movements (e.g. in wood)
- Mechanical properties of gypsum
- Shear strength of concrete



